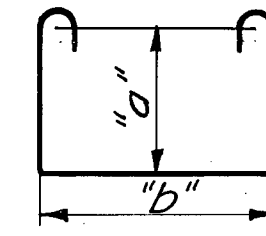
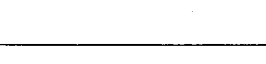
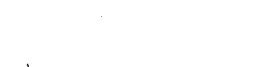
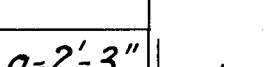
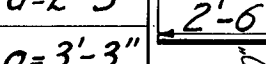
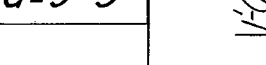
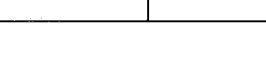
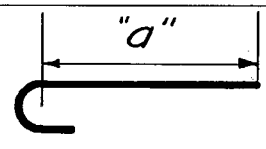
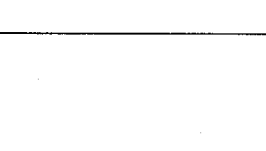
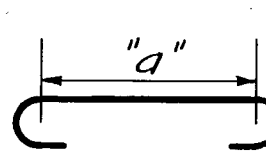
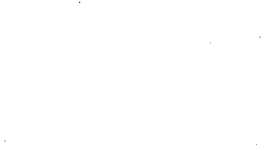
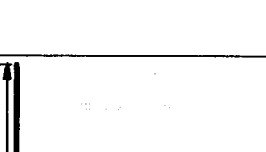
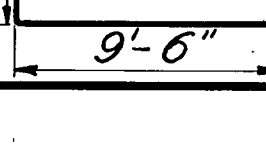


MARK	SIZE	LENGTH	BENDING DIAGRAM	NO REQ'D	WT. PER FOOT	TOTAL WEIGHT	LOCATION	MARK	SIZE	LENGTH	BENDING DIAGRAM	NO. REQ'D	WT. PER FOOT	TOTAL WEIGHT	LOCATION	MARK	SIZE	LENGTH	BENDING DIAGRAM	NO. REQ'D	WT. PER FOOT	TOTAL WEIGHT	LOCATION
A 1	$\frac{1}{2}$ " $\square$	33'-9"	<i>Straight</i>	138	.850	3959	Flume - longitudinal	A 68	$\frac{1}{2}$ " $\square$	34'-0"	<i>Straight</i>	2	.850	58	Base - longitudinal	CB 1	$\frac{3}{8}$ " ϕ	25'-6"		148	2.044	7,714	Flume
A 2	$\frac{1}{2}$ " $\square$	27'-6"	<i>do</i>	32	.850	748	<i>do</i>	A 69	$\frac{1}{2}$ " $\square$	9'-6"	<i>do</i>	2	.850	16	<i>do</i>	CB 2	$\frac{3}{8}$ " ϕ	25'-10'		2	2.044	106	<i>do</i>
A 3	$\frac{3}{8}$ " ϕ	20'-0"	<i>do</i>	2	2.044	82	Base - transverse	A 70	$\frac{3}{8}$ " ϕ	9'-9"	<i>do</i>	60	2.044	1,196	Base - transverse	CB 3	$\frac{3}{8}$ " ϕ	26'-2"		2	2.044	107	<i>do</i>
A 4	$\frac{1}{4}$ " $\square$	20'-0"	<i>do</i>	4	5.313	425	<i>do</i>	A 71	$\frac{1}{4}$ " $\square$	15'-6"	<i>do</i>	16	5.313	1318	<i>do</i>	CB 4	$\frac{3}{8}$ " ϕ	26'-9"		2	2.044	109	<i>do</i>
A 5	$\frac{3}{8}$ " ϕ	4'-6"	<i>do</i>	4	2.044	37	<i>do</i>	A 72	$\frac{1}{4}$ " $\square$	14'-0"	<i>do</i>	16	5.313	1,190	<i>do</i>	CB 5	$\frac{3}{8}$ " ϕ	27'-2"		2	2.044	111	<i>do</i>
A 6	$\frac{1}{4}$ " $\square$	4'-6"	<i>do</i>	4	5.313	96	<i>do</i>	A 73	$\frac{1}{4}$ " $\square$	5'-0"	<i>do</i>	7	5.313	186	<i>do</i>	CB 6	$\frac{3}{8}$ " ϕ	27'-9"		2	2.044	113	<i>do</i>
A 7	$\frac{3}{8}$ " ϕ	11'-6"	<i>do</i>	8	2.044	188	<i>do</i>	A 74	$\frac{1}{4}$ " $\square$	5'-0"	<i>do</i>	7	5.313	223	<i>do</i>	CB 7	$\frac{3}{8}$ " ϕ	28'-2"		2	2.044	115	<i>do</i>
A 8	$\frac{1}{4}$ " $\square$	8'-0"	<i>do</i>	8	5.313	340	<i>do</i>	A 75	$\frac{1}{4}$ " $\square$	16'-0"	<i>do</i>	5	5.313	425	<i>do</i>	CB 8	$\frac{3}{8}$ " ϕ	28'-9"		2	2.044	118	<i>do</i>
A 9	$\frac{3}{8}$ " ϕ	16'-3"	<i>do</i>	8	2.044	266	<i>do</i>	A 76	$\frac{1}{4}$ " $\square$	17'-3"	<i>do</i>	31	5.313	2,841	<i>do</i>	CB 9	$\frac{3}{8}$ " ϕ	29'-2"		3	2.044	179	<i>do</i>
A 10	$\frac{1}{4}$ " $\square$	19'-9"	<i>do</i>	15	5.313	1,574	<i>do</i>	A 77	$\frac{1}{4}$ " $\square$	15'-6"	<i>do</i>	31	5.313	2,553	<i>do</i>	CB 10	$\frac{3}{8}$ " ϕ	29'-10'		3	2.044	183	<i>do</i>
A 11	$\frac{3}{8}$ " ϕ	5'-3"	<i>do</i>	4	2.044	43	<i>do</i>	A 78	$\frac{1}{4}$ " $\square$	8'-0"	<i>do</i>	4	5.313	170	<i>do</i>	CB 11	$\frac{3}{8}$ " ϕ	30'-6"		3	2.044	187	<i>do</i>
A 12	$\frac{1}{4}$ " $\square$	5'-3"	<i>do</i>	4	5.313	112	<i>do</i>	A 79	$\frac{1}{4}$ " $\square$	11'-9"	<i>do</i>	4	5.313	250	<i>do</i>	CB 12	$\frac{3}{8}$ " ϕ	29'-9"		3	2.044	182	<i>do</i>
A 13	$\frac{3}{8}$ " ϕ	19'-3"	<i>do</i>	23	2.044	905	<i>do</i>	A 80	$\frac{3}{8}$ " ϕ	18'-9"	<i>do</i>	16	2.044	613	<i>do</i>	CB 13	$\frac{3}{8}$ " ϕ	30'-8"		3	2.044	188	<i>do</i>
A 14	1" $\square$	10'-3"	<i>do</i>	68	3.400	2,370	<i>do</i>	A 81	1" $\square$	10'-3"	<i>do</i>	16	3.400	558	<i>do</i>	CB 14	$\frac{3}{8}$ " ϕ	31'-7"		3	2.044	194	<i>do</i>
A 15	$\frac{3}{8}$ " ϕ	10'-3"	<i>do</i>	68	2.044	1,425	<i>do</i>	A 82	1" $\square$	10'-3"	<i>do</i>	14	3.400	488	<i>do</i>	CB 15	$\frac{3}{8}$ " ϕ	31'-4"		3	2.044	192	<i>do</i>
A 16	$\frac{1}{4}$ " $\square$	15'-9"	<i>do</i>	19	5.313	1,590	<i>do</i>	A 83	$\frac{3}{8}$ " ϕ	19'-3"	<i>do</i>	4	2.044	157	<i>do</i>	CB 16	$\frac{3}{8}$ " ϕ	32'-0"		3	2.044	196	<i>do</i>
A 17	$\frac{1}{4}$ " $\square$	13'-9"	<i>do</i>	18	5.313	1,315	<i>do</i>	A 84	$\frac{3}{8}$ " ϕ	20'-6"	<i>do</i>	31	2.044	1,299	<i>do</i>	CB 17	$\frac{3}{8}$ " ϕ	32'-8"		3	2.044	200	<i>do</i>
A 18	$\frac{1}{2}$ " $\square$	21'-3"	<i>do</i>	3	.850	54	Base - longitudinal	A 85	1" $\square$	10'-0"	<i>do</i>	36	3.400	1,224	<i>do</i>								
A 19	$\frac{1}{2}$ " $\square$	21'-9"	<i>do</i>	3	.850	55	<i>do</i>	A 86	$\frac{3}{8}$ " ϕ	9'-6"	<i>do</i>	3	2.044	58	<i>do</i>								
A 20	$\frac{1}{2}$ " $\square$	3'-9"	<i>do</i>	3	.850	10	<i>do</i>	A 87	$\frac{3}{8}$ " ϕ	16'-0"	<i>do</i>	3	2.044	98	<i>do</i>								
A 21	$\frac{1}{2}$ " $\square$	4'-9"	<i>do</i>	3	.850	12	<i>do</i>	A 88	$\frac{1}{2}$ " $\square$	12'-6"	<i>do</i>	40	.850	425	Base - longitudinal								
A 22	$\frac{1}{2}$ " $\square$	1'-3"	<i>do</i>	3	.850	3	<i>do</i>	A 89	$\frac{1}{2}$ " $\square$	29'-6"	<i>do</i>	2	.850	50	<i>do</i>								
A 23	$\frac{3}{8}$ " ϕ	19'-0"	<i>do</i>	34	2.044	1,320	Base - transverse	A 90	$\frac{1}{2}$ " $\square$	12'-0"	<i>do</i>	8	.850	82	<i>do</i>								
A 24	$\frac{1}{4}$ " $\square$	15'-7"	<i>do</i>	34	5.313	2,814	<i>do</i>	A 91	$\frac{1}{2}$ " $\square$	11'-0"	<i>do</i>	8	.850	75	<i>do</i>								
A 25	$\frac{1}{4}$ " $\square$	13'-7"	<i>do</i>	34	5.313	2,453	<i>do</i>	A 92	$\frac{1}{2}$ " $\square$	9'-0"	<i>do</i>	8	.850	61	<i>do</i>								
A 26	$\frac{3}{8}$ " ϕ	17'-6"	<i>do</i>	14	2.044	501	<i>do</i>	A 93	$\frac{1}{2}$ " $\square$	7'-0"	<i>do</i>	10	.850	60	<i>do</i>								
A 27	$\frac{3}{8}$ " ϕ	17'-0"	<i>do</i>	14	2.044	486	<i>do</i>	A 94	$\frac{1}{2}$ " $\square$	6'-0"	<i>do</i>	8	.850	41	<i>do</i>								
A 28	1" $\square$	8'-9"	<i>do</i>	27	3.400	803	<i>do</i>	A 81	$\frac{1}{2}$ " $\square$	7'-9"		12	.850	79	Flume								
A 29	1" $\square$	8'-9"	<i>do</i>	28	3.400	833	<i>do</i>	A 82	1" $\square$	8'-1"		430	3.400	11,813	Dowels-riverside stem								
A 30	$\frac{1}{4}$ " $\square$	13'-6"	<i>do</i>	28	5.313	2,008	<i>do</i>	A 83	1" $\square$	9'-1"		208	3.400	6,421	<i>do</i>								
A 31	$\frac{1}{4}$ " $\square$	11'-6"	<i>do</i>	28	5.313	1,711	<i>do</i>	AC 1	$\frac{5}{8}$ " ϕ	12'-2"		148	1.043	1,879	Flume								
A 32	$\frac{1}{2}$ " $\square$	27'-6"	<i>do</i>	36	.850	842	Base - longitudinal	AC 2	$\frac{5}{8}$ " ϕ	8'-7"		296	1.043	2,649	<i>do</i>								
A 33	$\frac{3}{8}$ " ϕ	6'-0"	<i>do</i>	207	2.044	2,539	Dowels-landside stem	AC 3	$\frac{3}{8}$ " ϕ	11'-7"		3	2.044	71	<i>do</i>								
								AC 4	$\frac{5}{8}$ " ϕ	8'-8"		7	1.043	63	<i>do</i>								
A 35	$\frac{1}{2}$ " $\square$	36'-0"	<i>do</i>	6	.850	184	Flume - longitudinal	AC 5	$\frac{5}{8}$ " ϕ	8'-11"		7	1.043	65	<i>do</i>								
A 36	$\frac{1}{2}$ " $\square$	9'-0"	<i>do</i>	6	.850	46	<i>do</i>	AC 6	$\frac{5}{8}$ " ϕ	9'-2"		7	1.043	67	<i>do</i>								
A 37	$\frac{1}{2}$ " $\square$	8'-0"	<i>do</i>	10	.850	68	<i>do</i>	AC 7	$\frac{5}{8}$ " ϕ	9'-5"		7	1.043	69	<i>do</i>								
A 38	$\frac{1}{2}$ " $\square$	35'-0"	<i>do</i>	10	.850	298	<i>do</i>	AC 8	$\frac{5}{8}$ " ϕ	9'-11"		7	1.043	72	<i>do</i>								
A 39	$\frac{1}{2}$ " $\square$	23'-0"	<i>do</i>	2	.850	39	<i>do</i>	AC 9	$\frac{5}{8}$ " ϕ	10'-2"		7	1.043	74	<i>do</i>								
								AC 10	$\frac{5}{8}$ " ϕ	10'-5"		7	1.043	77	<i>do</i>								
A 50	$\frac{1}{4}$ " $\square$	14'-6"	<i>do</i>	10	5.313	770	Base - transverse	AC 11	$\frac{5}{8}$ " ϕ	10'-11"		7	1.043	80	<i>do</i>								
A 51	$\frac{1}{4}$ " $\square$	13'-6"	<i>do</i>	10	5.313	717	<i>do</i>	AC 12	$\frac{5}{8}$ " ϕ	11'-2"		7	1.043	82	<i>do</i>								
A 52	$\frac{1}{4}$ " $\square$	14'-0"	<i>do</i>	10	5.313	744	<i>do</i>	AC 13	$\frac{5}{8}$ " ϕ	11'-5"		7	1.043	83	<i>do</i>								
A 53	$\frac{1}{4}$ " $\square$	14'-3"	<i>do</i>	10	5.313	757	<i>do</i>	AC 14	$\frac{5}{8}$ " ϕ	11'-8"		7	1.043	85	<i>do</i>								
A 54	$\frac{1}{4}$ " $\square$	14'-9"	<i>do</i>	12	5.313	940	<i>do</i>	AC 15	$\frac{5}{8}$ " ϕ	11'-11"		7	1.043	87	<i>do</i>								
A 55	$\frac{1}{4}$ " $\square$	13'-0"	<i>do</i>	9	5.313	622	<i>do</i>	AC 16	$\frac{5}{8}$ " ϕ	12'-2"		7	1.043	89	<i>do</i>								
A 56	$\frac{1}{4}$ " $\square$	13'-6"	<i>do</i>	42	5.313	3,012	<i>do</i>	AC 17	$\frac{5}{8}$ " ϕ	12'-5"		8	1.043	104	<i>do</i>								
A 57	$\frac{3}{8}$ " ϕ	9'-0"	<i>do</i>	52	2.044	957	<i>do</i>	AC 21	$\frac{5}{8}$ " ϕ	12'-8"		10	1.043	132	<i>do</i>								
A 58	$\frac{3}{8}$ " ϕ	17'-9"	<i>do</i>	10	2.044	363	<i>do</i>	AC 22	$\frac{5}{8}$ " $\$														