

MARK	SIZE	LENGTH	BENDING DIAGRAM	NO REQ'D	WT. PER FOOT	TOTAL WEIGHT	LOCATION	MARK	SIZE	LENGTH	BENDING DIAGRAM	NO. REQ'D	WT. PER FOOT	TOTAL WEIGHT	LOCATION	MARK	SIZE	LENGTH	BENDING DIAGRAM	NO. REQ'D	WT. PER FOOT	TOTAL WEIGHT	LOCATION	
A 1	$\frac{1}{2}$ " $\square$	33'-9"	<i>Straight</i>	138	.850	3959	Flume - longitudinal	A 68	$\frac{1}{2}$ " $\square$	34'-0"	<i>Straight</i>	2	.850	58	Base - longitudinal	CB 1	$\frac{3}{8}$ " ϕ	25'-6"		148	2.044	774	Flume	
A 2	$\frac{1}{2}$ " $\square$	27'-6"	<i>do</i>	32	.850	748	<i>do</i>	A 69	$\frac{1}{2}$ " $\square$	9'-6"	<i>do</i>	2	.850	16	<i>do</i>	CB 2	$\frac{3}{8}$ " ϕ	25'-10"		2	2.044	106	<i>do</i>	
A 3	$\frac{3}{8}$ " ϕ	20'-0"	<i>do</i>	2	2.044	82	Base - transverse	A 70	$\frac{3}{8}$ " ϕ	9'-9"	<i>do</i>	60	2.044	1196	Base - transverse	CB 3	$\frac{3}{8}$ " ϕ	26'-2"		2	2.044	107	<i>do</i>	
A 4	$\frac{1}{4}$ " ϕ	20'-0"	<i>do</i>	4	5.313	425	<i>do</i>	A 71	$\frac{1}{4}$ " ϕ	15'-6"	<i>do</i>	16	5.313	1318	<i>do</i>	CB 4	$\frac{3}{8}$ " ϕ	26'-9"		2	2.044	109	<i>do</i>	
A 5	$\frac{1}{8}$ " ϕ	4'-6"	<i>do</i>	4	2.044	37	<i>do</i>	A 72	$\frac{1}{4}$ " ϕ	14'-0"	<i>do</i>	16	5.313	1190	<i>do</i>	CB 5	$\frac{3}{8}$ " ϕ	27'-2"		2	2.044	111	<i>do</i>	
A 6	$\frac{1}{4}$ " ϕ	4'-6"	<i>do</i>	4	5.313	96	<i>do</i>	A 73	$\frac{1}{4}$ " ϕ	5'-0"	<i>do</i>	7	5.313	186	<i>do</i>	CB 6	$\frac{3}{8}$ " ϕ	27'-9"		2	2.044	113	<i>do</i>	
A 7	$\frac{3}{8}$ " ϕ	11'-6"	<i>do</i>	8	2.044	188	<i>do</i>	A 74	$\frac{1}{4}$ " ϕ	6'-0"	<i>do</i>	7	5.313	223	<i>do</i>	CB 7	$\frac{3}{8}$ " ϕ	28'-2"		2	2.044	115	<i>do</i>	
A 8	$\frac{1}{4}$ " ϕ	8'-0"	<i>do</i>	8	5.313	340	<i>do</i>	A 75	$\frac{1}{4}$ " ϕ	16'-0"	<i>do</i>	5	5.313	425	<i>do</i>	CB 8	$\frac{3}{8}$ " ϕ	28'-9"		2	2.044	118	<i>do</i>	
A 9	$\frac{3}{8}$ " ϕ	16'-3"	<i>do</i>	8	2.044	266	<i>do</i>	A 76	$\frac{1}{4}$ " ϕ	17'-3"	<i>do</i>	31	5.313	2841	<i>do</i>	CB 9	$\frac{3}{8}$ " ϕ	29'-2"		3	2.044	179	<i>do</i>	
A 10	$\frac{1}{4}$ " ϕ	19'-9"	<i>do</i>	15	5.313	1574	<i>do</i>	A 77	$\frac{1}{4}$ " ϕ	15'-6"	<i>do</i>	31	5.313	2553	<i>do</i>	CB 10	$\frac{3}{8}$ " ϕ	29'-10"		3	2.044	183	<i>do</i>	
A 11	$\frac{3}{8}$ " ϕ	5'-3"	<i>do</i>	4	2.044	43	<i>do</i>	A 78	$\frac{1}{4}$ " ϕ	8'-0"	<i>do</i>	4	5.313	170	<i>do</i>	CB 11	$\frac{3}{8}$ " ϕ	30'-6"		3	2.044	187	<i>do</i>	
A 12	$\frac{1}{4}$ " ϕ	5'-3"	<i>do</i>	4	5.313	112	<i>do</i>	A 79	$\frac{1}{4}$ " ϕ	11'-9"	<i>do</i>	4	5.313	250	<i>do</i>	CB 12	$\frac{3}{8}$ " ϕ	29'-9"		3	2.044	182	<i>do</i>	
A 13	$\frac{3}{8}$ " ϕ	19'-3"	<i>do</i>	23	2.044	905	<i>do</i>	A 80	$\frac{3}{8}$ " ϕ	18'-9"	<i>do</i>	16	2.044	613	<i>do</i>	CB 13	$\frac{3}{8}$ " ϕ	30'-8"		3	2.044	188	<i>do</i>	
A 14	$\frac{1}{2}$ " ϕ	10'-3"	<i>do</i>	68	3.400	2370	<i>do</i>	A 81	$\frac{1}{2}$ " ϕ	10'-3"	<i>do</i>	16	3.400	558	<i>do</i>	CB 14	$\frac{3}{8}$ " ϕ	31'-7"		3	2.044	194	<i>do</i>	
A 15	$\frac{3}{8}$ " ϕ	10'-3"	<i>do</i>	68	2.044	1425	<i>do</i>	A 82	$\frac{1}{2}$ " ϕ	10'-3"	<i>do</i>	14	3.400	488	<i>do</i>	CB 15	$\frac{3}{8}$ " ϕ	31'-4"		3	2.044	192	<i>do</i>	
A 16	$\frac{1}{4}$ " ϕ	15'-9"	<i>do</i>	19	5.313	1590	<i>do</i>	A 83	$\frac{3}{8}$ " ϕ	19'-3"	<i>do</i>	4	2.044	157	<i>do</i>	CB 16	$\frac{3}{8}$ " ϕ	32'-0"		3	2.044	196	<i>do</i>	
A 17	$\frac{1}{4}$ " ϕ	13'-9"	<i>do</i>	18	5.313	1315	<i>do</i>	A 84	$\frac{3}{8}$ " ϕ	20'-6"	<i>do</i>	31	2.044	1299	<i>do</i>	CB 17	$\frac{3}{8}$ " ϕ	32'-8"		3	2.044	200	<i>do</i>	
A 18	$\frac{1}{2}$ " ϕ	21'-3"	<i>do</i>	3	.850	54	Base - longitudinal	A 85	$\frac{1}{2}$ " ϕ	10'-0"	<i>do</i>	36	3.400	1224	<i>do</i>									
A 19	$\frac{1}{2}$ " ϕ	21'-9"	<i>do</i>	3	.850	55	<i>do</i>	A 86	$\frac{3}{8}$ " ϕ	9'-6"	<i>do</i>	3	2.044	58	<i>do</i>									
A 20	$\frac{1}{2}$ " ϕ	3'-9"	<i>do</i>	3	.850	10	<i>do</i>	A 87	$\frac{3}{8}$ " ϕ	16'-0"	<i>do</i>	3	2.044	98	<i>do</i>									
A 21	$\frac{1}{2}$ " ϕ	4'-9"	<i>do</i>	3	.850	12	<i>do</i>	A 88	$\frac{1}{2}$ " ϕ	12'-6"	<i>do</i>	40	.850	425	Base - longitudinal									
A 22	$\frac{1}{2}$ " ϕ	1'-3"	<i>do</i>	3	.850	3	<i>do</i>	A 89	$\frac{1}{2}$ " ϕ	29'-6"	<i>do</i>	2	.850	50	<i>do</i>									
A 23	$\frac{3}{8}$ " ϕ	19'-0"	<i>do</i>	34	2.044	1320	Base - transverse	A 90	$\frac{1}{2}$ " ϕ	12'-0"	<i>do</i>	8	.850	82	<i>do</i>	K 1	$\frac{3}{8}$ " ϕ	10'-4"		120	1.502	1862	Pile bars	
A 24	$\frac{1}{4}$ " ϕ	15'-7"	<i>do</i>	34	5.313	2814	<i>do</i>	A 91	$\frac{1}{2}$ " ϕ	11'-0"	<i>do</i>	8	.850	75	<i>do</i>	K 2	$\frac{3}{8}$ " ϕ	11'-4"		39	1.502	664	<i>do</i>	
A 25	$\frac{1}{4}$ " ϕ	13'-7"	<i>do</i>	34	5.313	2453	<i>do</i>	A 92	$\frac{1}{2}$ " ϕ	9'-0"	<i>do</i>	8	.850	61	<i>do</i>									
A 26	$\frac{3}{8}$ " ϕ	17'-6"	<i>do</i>	14	2.044	501	<i>do</i>	A 93	$\frac{1}{2}$ " ϕ	7'-0"	<i>do</i>	10	.850	60	<i>do</i>									
A 27	$\frac{1}{8}$ " ϕ	17'-0"	<i>do</i>	14	2.044	486	<i>do</i>	A 94	$\frac{1}{2}$ " ϕ	6'-0"	<i>do</i>	8	.850	41	<i>do</i>									
A 28	$\frac{1}{2}$ " ϕ	8'-9"	<i>do</i>	27	3.400	803	<i>do</i>	A B 1	$\frac{1}{2}$ " ϕ	7'-9"		12	.850	79	Flume									
A 29	$\frac{1}{2}$ " ϕ	8'-9"	<i>do</i>	28	3.400	833	<i>do</i>	A B 2	$\frac{1}{2}$ " ϕ	8'-1"		430	3.400	11,813	Dowels-riverside stem									
A 30	$\frac{1}{4}$ " ϕ	13'-6"	<i>do</i>	28	5.313	2008	<i>do</i>	A B 3	$\frac{1}{2}$ " ϕ	9'-1"		208	3.400	6,421	<i>do</i>									
A 31	$\frac{1}{4}$ " ϕ	11'-6"	<i>do</i>	28	5.313	1711	<i>do</i>	A C 1	$\frac{5}{8}$ " ϕ	12'-2"		148	1.043	1,879	Flume									
A 32	$\frac{1}{2}$ " ϕ	27'-6"	<i>do</i>	36	.850	842	Base - longitudinal	A C 2	$\frac{5}{8}$ " ϕ	8'-7"		296	1.043	2,649	<i>do</i>									
A 33	$\frac{3}{8}$ " ϕ	6'-0"	<i>do</i>	207	2.044	2539	Dowels-landside stem	A C 3	$\frac{5}{8}$ " ϕ	11'-7"		3	2.044	71	<i>do</i>									
A 35	$\frac{1}{2}$ " ϕ	36'-0"	<i>do</i>	6	.850	184	Flume - longitudinal	A C 4	$\frac{5}{8}$ " ϕ	8'-8"		7	1.043	63	<i>do</i>									
A 36	$\frac{1}{2}$ " ϕ	9'-0"	<i>do</i>	6	.850	46	<i>do</i>	A C 5	$\frac{5}{8}$ " ϕ	8'-11"		7	1.043	65	<i>do</i>									
A 37	$\frac{1}{2}$ " ϕ	8'-0"	<i>do</i>	10	.850	68	<i>do</i>	A C 6	$\frac{5}{8}$ " ϕ	9'-2"		7	1.043	67	<i>do</i>									
A 38	$\frac{1}{2}$ " ϕ	35'-0"	<i>do</i>	10	.850	298	<i>do</i>	A C 7	$\frac{5}{8}$ " ϕ	9'-5"		7	1.043	69	<i>do</i>									
A 39	$\frac{1}{2}$ " ϕ	23'-0"	<i>do</i>	2	.850	39	<i>do</i>	A C 8	$\frac{5}{8}$ " ϕ	9'-11"		7	1.043	72	<i>do</i>									
A 50	$\frac{1}{4}$ " ϕ	14'-6"	<i>do</i>	10	5.313	770	Base - transverse	A C 9	$\frac{5}{8}$ " ϕ	10'-2"		7	1.043	74	<i>do</i>									
A 51	$\frac{1}{4}$ " ϕ	13'-6"	<i>do</i>	10	5.313	717	<i>do</i>	A C 10	$\frac{5}{8}$ " ϕ	10'-5"		7	1.043	77	<i>do</i>									
A 52	$\frac{1}{4}$ " ϕ	14'-0"	<i>do</i>	10	5.313	744	<i>do</i>	A C 11	$\frac{5}{8}$ " ϕ	10'-11"		7	1.043	80	<i>do</i>									
A 53	$\frac{1}{4}$ " ϕ	14'-3"	<i>do</i>	10	5.313	757	<i>do</i>	A C 12	$\frac{5}{8}$ " ϕ	11'-2"		7	1.043	82	<i>do</i>									
A 54	$\frac{1}{4}$ " ϕ	14'-9"	<i>do</i>	12	5.313	940	<i>do</i>	A C 13	$\frac{5}{8}$ " ϕ	11'-5"		7	1.043	83	<i>do</i>									
A 55	$\frac{1}{4}$ " ϕ	13'-0"	<i>do</i>	9	5.313	622	<i>do</i>	A C 14	$\frac{5}{8}$ " ϕ	11'-8"		7	1.043	85	<i>do</i>									
A 56	$\frac{1}{4}$ " ϕ	13'-6"	<i>do</i>	42	5.313	3012	<i>do</i>	A C 15	$\frac{5}{8}$ " ϕ	11'-11"		7	1.043	87	<i>do</i>									
A 57	$\frac{3}{8}$ " ϕ	9'-0"	<i>do</i>	52	2.044	957	<i>do</i>	A C 16	$\frac{5}{8}$ " ϕ	12'-2"		7	1.043	89	<i>do</i>									
A 58	$\frac{3}{8}$ " ϕ	17'-9"	<i>do</i>	10	2.044	363	<i>do</i>	A C 17	$\frac{5}{8}$ " ϕ	12'-5"		8	1.043	104	<i>do</i>									
A 59	$\frac{3}{8}$ " ϕ	16'-9"	<i>do</i>	14	2.044	479	<i>do</i>	A C 21	$\frac{5}{8}$ " ϕ	12'-8"		10	1.043	132	<i>do</i>									
A 60	$\frac{3}{8}$ " ϕ	17'-3"	<i>do</i>	14	2.044	494	<i>do</i>	A C 22	$\frac{5}{8}$ " ϕ	11'-8"		5	1.043	61	<i>do</i>									
A 61	$\frac{3}{8}$ " ϕ	18'-0"	<i>do</i>	14	2.044	515	<i>do</i>	A C 2																