

REINFORCEMENT SCHEDULE

MARK	SIZE	LENGTH	BENDING DIAGRAM		NO. REQ'D	WT. EACH	TOTAL WT.	MARK	SIZE	LENGTH	BENDING DIAGRAM		NO. REQ'D	WT. EACH	TOTAL WT.	MARK	SIZE	LENGTH	BENDING DIAGRAM		NO. REQ'D	WT. EACH	TOTAL WT.
058-0AA	$\frac{5}{8}$ " ϕ	8'-0"			78	8.3	647	0510-0	$\frac{5}{8}$ " ϕ	10'-0"	Straight		3	10.4	31	0712-6EA	$\frac{7}{8}$ " ϕ	12'-6"			2	25.6	51
0511-9EA	$\frac{5}{8}$ " ϕ	11'-9"			120	12.3	1476	059-3	$\frac{5}{8}$ " ϕ	9'-3"	do		3	9.6	29	0711-9EA	$\frac{7}{8}$ " ϕ	11'-9"			3	24.0	72
0513-9EA	$\frac{5}{8}$ " ϕ	13'-9"			40	14.3	572	058-6	$\frac{5}{8}$ " ϕ	8'-6"	do		3	8.9	27	0711-6EA	$\frac{5}{8}$ " ϕ	11'-6"			3	23.5	71
0514-9EA	$\frac{5}{8}$ " ϕ	14'-9"			40	15.4	616	058-0	$\frac{5}{8}$ " ϕ	8'-0"	do		5	8.3	42	0711-0EA	$\frac{5}{8}$ " ϕ	11'-0"			3	22.5	68
059-9FA	$\frac{5}{8}$ " ϕ	9'-9"			237	10.2	2417	057-6	$\frac{5}{8}$ " ϕ	7'-6"	do		3	7.8	23	0710-6EA	$\frac{5}{8}$ " ϕ	10'-6"			3	21.5	65
0514-0BA	$\frac{5}{8}$ " ϕ	14'-0"		a=10'-5"	104	14.6	1518	057-0	$\frac{5}{8}$ " ϕ	7'-0"	do		7	7.3	51	0710-0EA	$\frac{5}{8}$ " ϕ	10'-0"			3	20.4	61
0513-6BA	$\frac{5}{8}$ " ϕ	13'-6"		a=9'-11"	4	14.1	56	056-6	$\frac{5}{8}$ " ϕ	6'-6"	do		3	6.8	20	079-3EA	$\frac{5}{8}$ " ϕ	9'-3"			1	18.9	19
0512-9BA	$\frac{5}{8}$ " ϕ	12'-9"		a=9'-2"	4	13.3	53	056-0	$\frac{5}{8}$ " ϕ	6'-0"	do		4	6.3	25	078-3FA	$\frac{5}{8}$ " ϕ	8'-3"			35	16.9	592
0512-0BA	$\frac{5}{8}$ " ϕ	12'-0"		a=8'-5"	4	12.5	50	055-9	$\frac{5}{8}$ " ϕ	5'-9"	do		5	6.0	30	078-9FA	$\frac{5}{8}$ " ϕ	8'-9"			78	17.9	1396
0511-3BA	$\frac{5}{8}$ " ϕ	11'-3"		a=7'-8"	4	11.7	47	055-0	$\frac{5}{8}$ " ϕ	5'-0"	do		6	5.2	31	079-0FA	$\frac{5}{8}$ " ϕ	9'-0"			79	18.4	1454
0511-0BA	$\frac{5}{8}$ " ϕ	11'-0"		a=7'-5"	120	11.5	1380	068-3AA	$\frac{3}{4}$ " ϕ	8'-3"			38	12.4	471	0713-0	$\frac{7}{8}$ " ϕ	13'-0"	Straight		78	26.6	2075
0510-9BA	$\frac{5}{8}$ " ϕ	10'-9"		a=7'-2"	4	11.2	45	0612-6EA	$\frac{5}{8}$ " ϕ	12'-6"			10	18.8	188	0813-0	1" ϕ	13'-0"	do		312	34.7	10826
0510-0BA	$\frac{5}{8}$ " ϕ	10'-0"		a=6'-5"	4	10.4	42	0612-3EA	$\frac{5}{8}$ " ϕ	12'-3"			10	18.4	184	0812-6	1" ϕ	12'-6"	do		6	33.4	200
059-3BA	$\frac{5}{8}$ " ϕ	9'-3"		a=5'-8"	4	9.6	38	0612-0EA	$\frac{5}{8}$ " ϕ	12'-0"			10	18.0	180	0812-0	1" ϕ	12'-0"	do		6	32.0	192
058-9BA	$\frac{5}{8}$ " ϕ	8'-9"		a=5'-2"	4	9.1	36	0611-9EA	$\frac{5}{8}$ " ϕ	11'-9"			10	17.6	176	0811-6	1" ϕ	11'-6"	do		6	30.7	184
058-0BA	$\frac{5}{8}$ " ϕ	8'-0"		a=4'-5"	4	8.3	33	068-9FA	$\frac{5}{8}$ " ϕ	8'-9"			80	13.1	1048	0811-0	1" ϕ	11'-0"	do		6	29.4	176
057-3BA	$\frac{5}{8}$ " ϕ	7'-3"		a=3'-8"	4	7.6	30	069-3FA	$\frac{5}{8}$ " ϕ	9'-3"			79	13.9	1098	0810-6	1" ϕ	10'-6"	do		6	28.0	168
0530-0	$\frac{5}{8}$ " ϕ	30'-0"	Straight		443	31.3	13866	069-6FA	$\frac{5}{8}$ " ϕ	9'-6"			79	14.3	1130	0810-0	1" ϕ	10'-0"	do		6	26.7	160
0529-6	$\frac{5}{8}$ " ϕ	29'-6"	do		2	30.8	62	067-0BA	$\frac{5}{8}$ " ϕ	7'-0"			44	10.5	462	064-9CA	$\frac{3}{4}$ " ϕ	4'-9"			221	7.1	1569
0524-0	$\frac{5}{8}$ " ϕ	24'-0"	do		22	25.0	550	0615-0BA	$\frac{5}{8}$ " ϕ	15'-0"			96	22.5	2160	Total Weight 68,586 pounds.							
0518-0	$\frac{5}{8}$ " ϕ	18'-0"	do		4	18.8	75	0610-0	$\frac{5}{8}$ " ϕ	10'-0"	Straight		234	15.0	3510								
0517-6	$\frac{5}{8}$ " ϕ	17'-6"	do		12	18.3	220	069-6	$\frac{5}{8}$ " ϕ	9'-6"	do		6	14.3	86								
0514-9	$\frac{5}{8}$ " ϕ	14'-9"	do		40	15.4	616	069-3	$\frac{5}{8}$ " ϕ	9'-3"	do		2	13.9	28								
0514-6	$\frac{5}{8}$ " ϕ	14'-6"	do		5	15.1	76	069-0	$\frac{5}{8}$ " ϕ	9'-0"	do		6	13.5	81								
0514-3	$\frac{5}{8}$ " ϕ	14'-3"	do		5	14.9	75	068-6	$\frac{5}{8}$ " ϕ	8'-6"	do		9	12.8	115								
0514-0	$\frac{5}{8}$ " ϕ	14'-0"	do		5	14.6	73	068-0	$\frac{5}{8}$ " ϕ	8'-0"	do		9	12.0	108								
0513-9	$\frac{5}{8}$ " ϕ	13'-9"	do		45	14.3	644	067-6	$\frac{5}{8}$ " ϕ	7'-6"	do		9	11.3	102								
0513-6	$\frac{5}{8}$ " ϕ	13'-6"	do		15	14.1	212	067-0	$\frac{5}{8}$ " ϕ	7'-0"	do		9	10.5	95								
0513-3	$\frac{5}{8}$ " ϕ	13'-3"	do		15	13.8	207	066-6	$\frac{5}{8}$ " ϕ	6'-6"	do		9	9.8	88								
0513-0	$\frac{5}{8}$ " ϕ	13'-0"	do		75	13.6	1020	065-9	$\frac{5}{8}$ " ϕ	5'-9"	do		5	8.6	43								
0512-9	$\frac{5}{8}$ " ϕ	12'-9"	do		17	13.3	226	078-6AA	$\frac{7}{8}$ " ϕ	8'-6"			96	17.4	1670								
0512-6	$\frac{5}{8}$ " ϕ	12'-6"	do		10	13.0	130	0714-6EA	$\frac{5}{8}$ " ϕ	14'-6"			5	29.6	148								
0512-3	$\frac{5}{8}$ " ϕ	12'-3"	do		10	12.8	128	0714-3EA	$\frac{5}{8}$ " ϕ	14'-3"			5	29.1	146								
0512-0	$\frac{5}{8}$ " ϕ	12'-0"	do		10	12.5	125	0714-0EA	$\frac{5}{8}$ " ϕ	14'-0"			5	28.6	143								
0511-9	$\frac{5}{8}$ " ϕ	11'-9"	do		133	12.3	1636	0713-9EA	$\frac{5}{8}$ " ϕ	13'-9"			5	28.1	141								
0511-6	$\frac{5}{8}$ " ϕ	11'-6"	do		384	12.0	4608	0713-6EA	$\frac{5}{8}$ " ϕ	13'-6"			5	27.6	138								
0511-0	$\frac{5}{8}$ " ϕ	11'-0"	do		3	11.5	35	0713-3EA	$\frac{5}{8}$ " ϕ	13'-3"			5	27.1	136								
0510-6	$\frac{5}{8}$ " ϕ	10'-6"	do		3	11.0	33	0713-0EA	$\frac{5}{8}$ " ϕ	13'-0"			5	26.6	133								
							0712-9EA	$\frac{5}{8}$ " ϕ	12'-9"			5	26.1	131									
							0713-5EA	$\frac{5}{8}$ " ϕ	13'-5"			10	27.4	274									
							0713-2EA	$\frac{5}{8}$ " ϕ	13'-2"			10	26.9	269									
							0712-11EA	$\frac{5}{8}$ " ϕ	12'-11"			10	26.4	264									
							0712-8EA	$\frac{5}{8}$ " ϕ	12'-8"			10	25.9	259									

NOTES
For steel details n
see sheets No. 3

NOTES
For steel details referring to this sheet,
see sheets No. 36 & 37.

CONNECTICUT RIVER FLOOD CONTROL			
NORTH MEADOWS DIKE			
FISCAL YEAR 1939 SECTION			
CONCRETE WALL			
REINFORCEMENT SCHEDULE			
HARTFORD, CONN.			
CONNECTICUT RIVER		CONNECTICUT	
IN 66 SHEETS		NOT TO SCALE SHEET NO. 38	
U. S. ENGINEER OFFICE, PROVIDENCE, R. I., APRIL 1939			
SUBMITTED: <i>Wm. B. Liden</i>		APPROVAL RECOMMENDED: <i>J. B. Burns</i>	
HEAD, DESIGN SECTION		PRINCIPAL ENGINEER	
DESIGNED: <i>J. C. Ingwall</i>		CHECKED: <i>J. S. M.</i>	
DATE: 12/31/45		REVISION: As-Built	
REV. BY: <i>J. C. Ingwall</i>		AP. BY: <i>J. S. M.</i>	
FILE NO. CT-4-1467			